

# Path optimization for the Laser Powder Bed Fusion (LPBF) additive manufacturing process

PhD funded by SOFIA project

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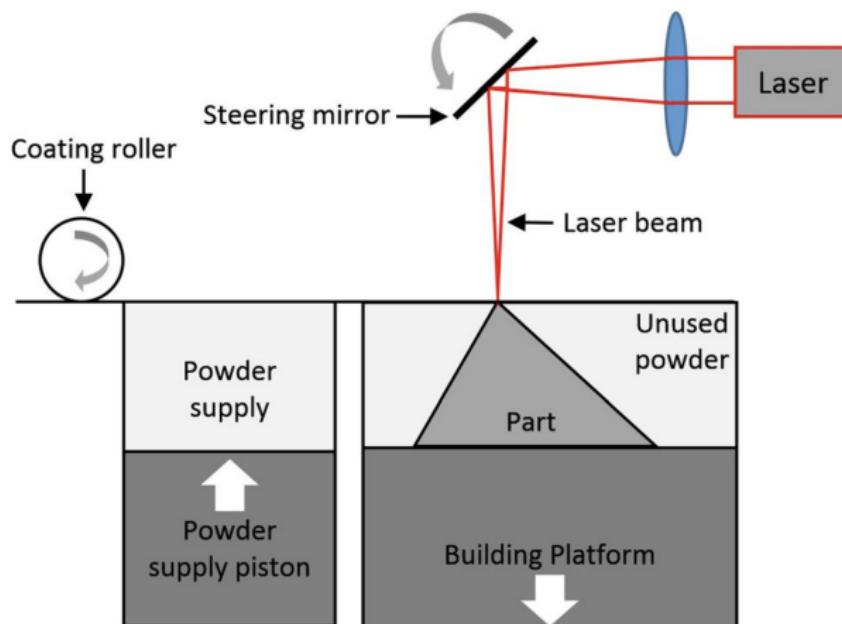
<sup>2</sup>LURPA, ENS Paris Saclay, France

12/09/2019



## Introduction

# The LPBF process

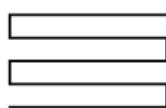


Process description (Bikas, Stavropoulos, and Chryssolouris 2016)

# Laser path

**State of the art : (Ding et al. 2015; Liu et al. 2018)**

parallel



contour



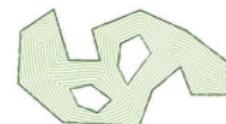
spiral



continuous



Medial Axis Transformation



- Allocation of these paths to domain cells,
- Velocity and power optimization,
- "Live" path adaptation.

**Goal : path optimization without basing it upon any pattern.**

# Outline

## 1 Introduction

## 2 Model

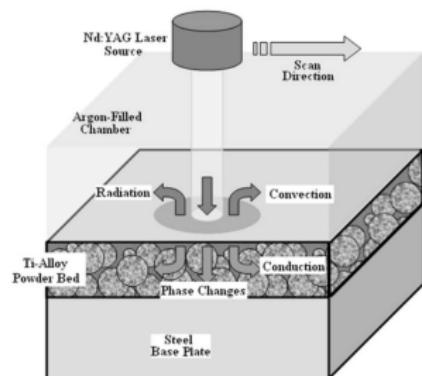
## 3 Steady problem

## 4 Unsteady problem

## 5 Conclusion and perspectives

## Model

# LPBF modelization



LPBF process  
(Roberts et al. 2009)

## Microscopic scale

(Megahed et al. 2016; DebRoy et al. 2018)

- accurate model for the change of state, melting pool,
- 4 states considered: powder, solid, liquid, gaz.

## Macroscopic scale

(Van Belle 2013; Megahed et al. 2016; Allaire and Jakabčin 2018)

- conduction, convection and radiation
- 2 states considered: powder and solid.

## Stakes at a macroscopic scale:

- **thermomechanics**: thermal expansion, residual stresses, solidification of the layer,
- **kinematics**: minimal execution time, easy to create.

# Macroscopic 2D model (in the layer plane)

## Heat equation (conduction only):

$$\begin{cases} \rho_{pow.} C_{p,pow.} \partial_t T - \nabla \cdot (\lambda_{pow.} \nabla T) + \frac{\lambda_{sol.}}{L \Delta Z} T = \frac{Q}{L}, & (t, x) \in (0, t_F) \times \Sigma, \\ \lambda_{pow.} \nabla T \cdot n = 0, & (t, x) \in (0, t_F) \times \partial\Sigma, \\ T(0, x) = T_{init}(x) & x \in \Sigma. \end{cases}$$

**Source model:**  $Q(t, x) = P \exp(-\delta|x - u(t)|^2)$ , ( $u(t)$  the laser path).

**Physical characteristics** time independent (powder or solid value chosen depending on the context).

## Constraints to satisfy:

- change of state:  $\forall x \in D, \exists t$  such that  $T(t, x) > T_\Phi$ ,
- thermal expansion:  $\forall x \in D, \forall t, T(t, x) < T_M$ ,
- residual stresses.

## Steady problem



# Optimization problem to consider

**Steady model:** source on the whole trajectory at the same time (heating thread).

**Objective :** vary the path  $\Gamma$  in order to minimize its length ( $J(\Gamma)$ ) while satisfying the change of phase ( $C_\Phi$ ) and maximal temperature constraints ( $C_M$ ).

$$\min_{\Gamma} J(\Gamma) = \int_{\Gamma} ds$$

while satisfying the constraints

$$\begin{cases} C_{\Phi,st} = \int_{\Sigma} [(T_{\Phi} - T)^+]^2 dx = 0 & (T > T_{\Phi}), \\ C_{M,st} = \int_{\Sigma} [(T - T_M)^+]^2 dx = 0 & (T < T_M). \end{cases}$$

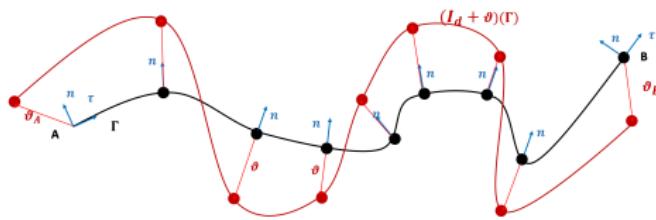
and  $T$  solution of:

$$\begin{cases} -\nabla \cdot (\lambda_{pow.} \nabla T) + \frac{\lambda_{sol.}}{L \Delta Z} T = \frac{P}{L} \chi_{\Gamma}, & (t, x) \in (0, t_F) \times \Sigma \\ \lambda_{pow.} \nabla T \cdot n = 0 & (t, x) \in (0, t_F) \times \partial \Sigma \end{cases}$$

# Computation of the speed of variation: shape optimization (Henrot and Pierre (2018) and Allaire, Jouve, and Toader (2004))

**Shape optimization:** variation with respect to a vector field  $\vartheta$ ,

$\Gamma$  regular curve with chosen orientation, which tangent is  $\tau$ , which normal is  $n$  and curvature  $\kappa$  with  $A$  and  $B$  its endpoints.



- Shape derivative of  $J(\Gamma) = \int_{\Gamma} f(s)ds$ :

$$J'(\Gamma)(\vartheta) = \int_{\Gamma} [\partial_n f + \kappa f] \vartheta \cdot n ds + f(B)\vartheta(B) \cdot \tau(B) - f(A)\vartheta(A) \cdot \tau(A)$$

- Then:

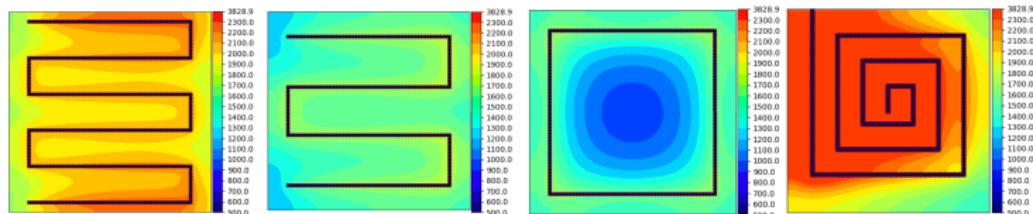
$$J(\Gamma^{n+1}) = J(\Gamma^n) + J'(\Gamma^n)(\vartheta) + o(\vartheta)$$

and  $\vartheta$  is chosen such that  $J(\Gamma^{n+1}) \leq J(\Gamma^n)$ .

# Results

**Values:** (Van Belle 2013; Allaire and Jakabčin 2018)

$$\begin{aligned} \lambda_{sol.} &= 15 W.m^{-1}K^{-1}, & \lambda_{pow.} &= 0.25 W.m^{-1}K^{-1}, & L &= 10cm, & \Delta Z &= 1m, & P &= 800 W.m^{-2}, \\ T_\Phi &= 1700K, & T_M &= 2000K, & T_{init} &= 500K. \end{aligned}$$



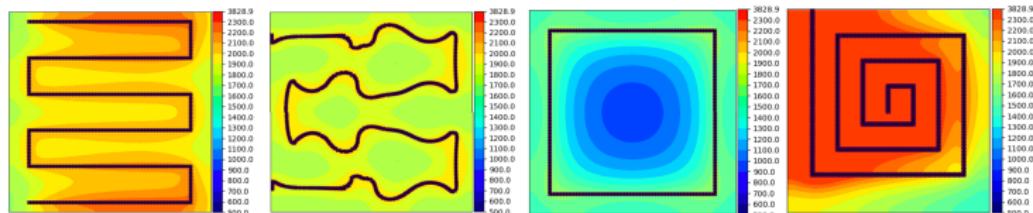
$$N(C_{\phi,st}) = \sqrt{\frac{C_{\phi,st}}{|\Sigma| T_\Phi^2}}, \quad N(C_{M,st}) = \sqrt{\frac{C_{M,st}}{|\Sigma| T_M^2}}$$

Case	Length (m)	$N(C_{\phi,st})$	$N(C_{M,st})$
Reference (non optimized)	1.14	$1.97e-5$	$3.29e-2$
Zigzag initialization	1.00	$3.63e-5$	$2.50e-5$
Contour initialization	1.00	$2.20e-4$	$2.92e-4$
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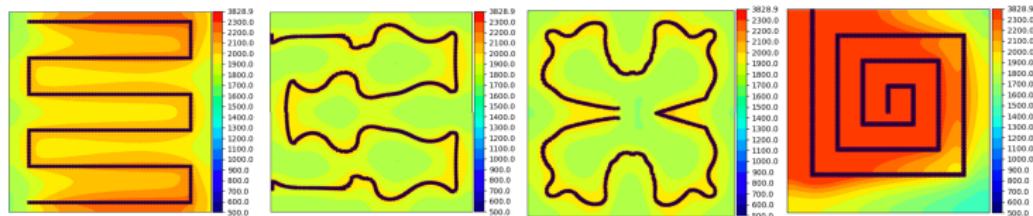
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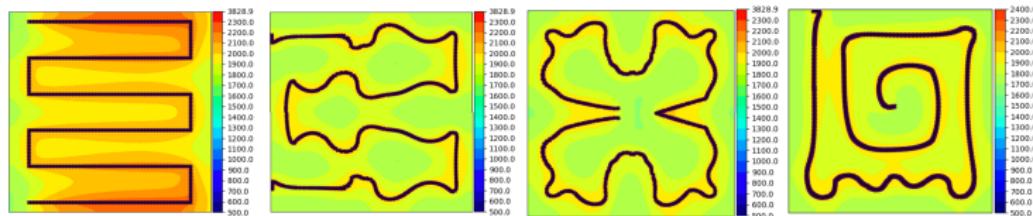
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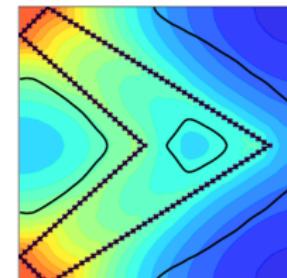
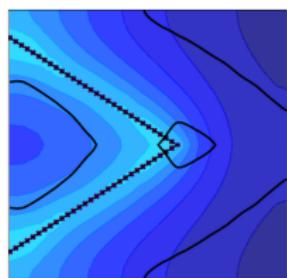
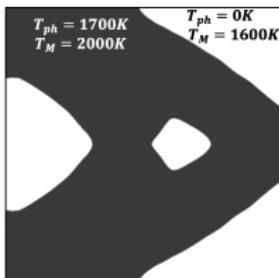


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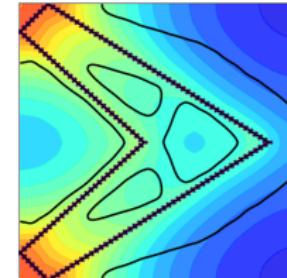
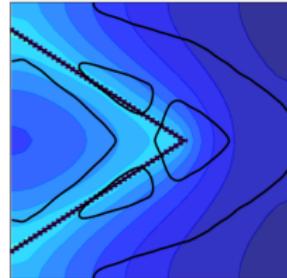
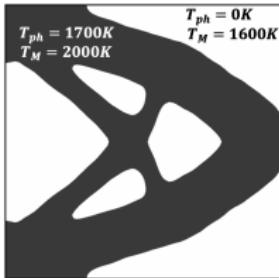
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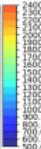
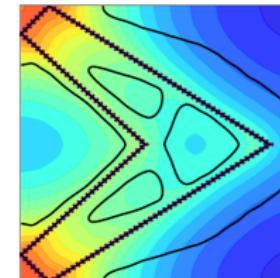
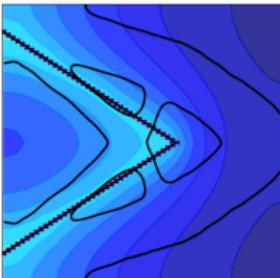
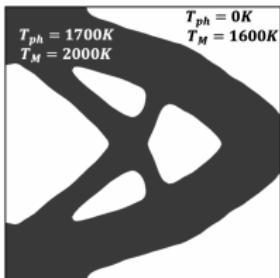
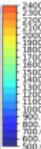
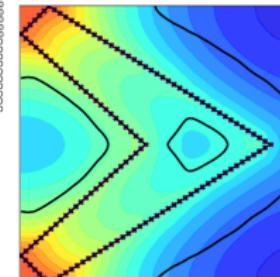
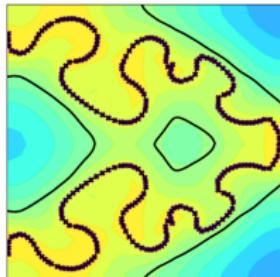
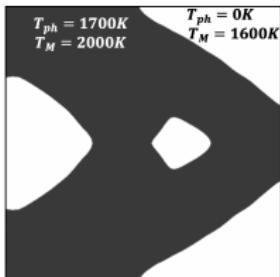


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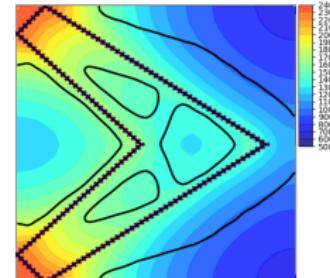
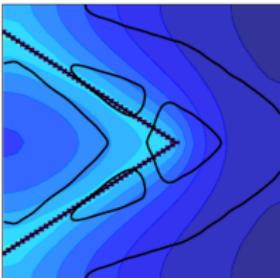
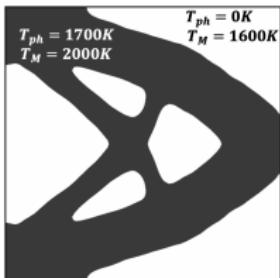
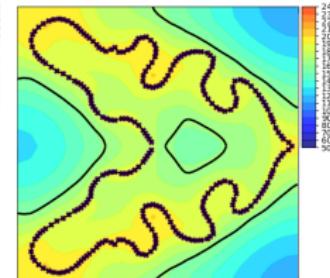
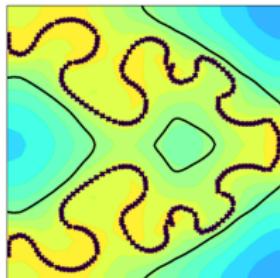
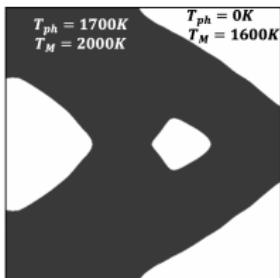


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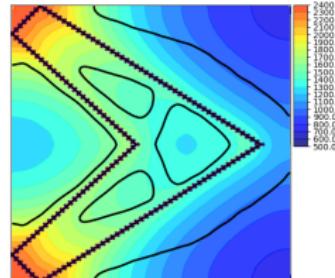
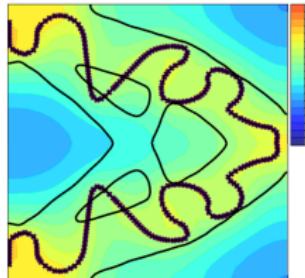
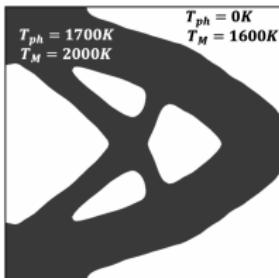
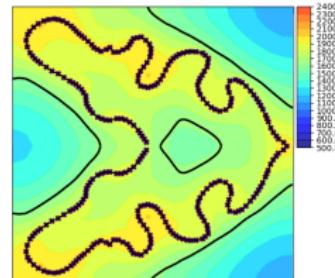
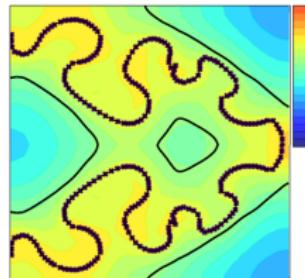
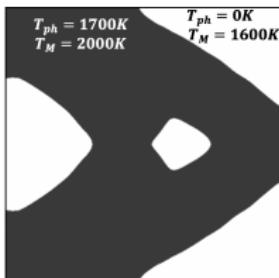
# Results



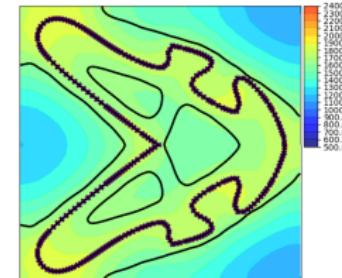
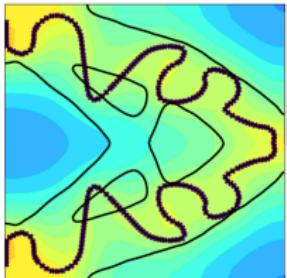
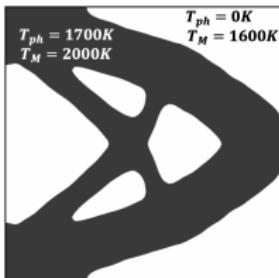
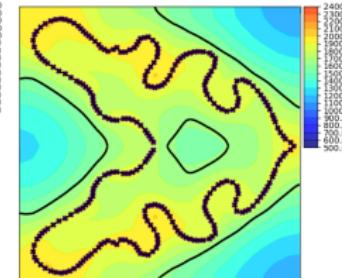
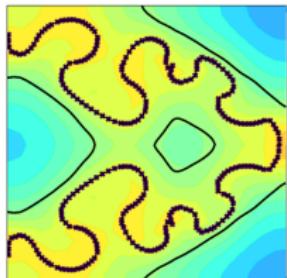
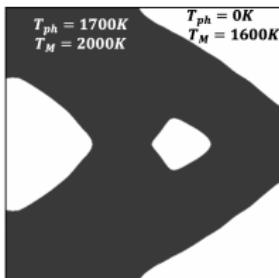
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## Unsteady problem

# Unsteady context (laser speed $V$ fixed)

**Objectives:** ■ final time:  $L_g = t_F$

■ change of state:  $\forall x \in D, \exists t \in [0, t_F]$  such that  $T(t, x) > T_\Phi$ ,

$$C_\Phi = \int_{\Sigma} \left[ \left( T_\Phi - \max_t (|T(., x)|) \right)^+ \right]^2 dx \approx \int_{\Sigma} \left[ (T_\Phi - \|T(., x)\|_{L^p(0, t_F)})^+ \right]^2 dx.$$

■ thermal expansion:  $\forall (x, t) \in \Sigma \times [0, t_F], T(t, x) < T_M$ ,

$$C_M = \int_{\Sigma} \int_0^{t_F} [(T(t, x) - T_M)^+]^2 dt dx.$$

**Equations:**

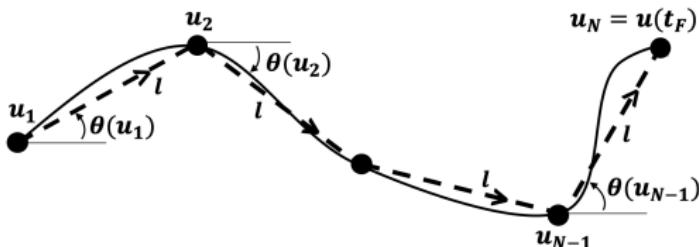
$$\begin{cases} \rho_{pow}.c_{p,pow}.\partial_t T - \nabla \cdot (\lambda_{pow}.\nabla T) + \frac{\lambda_{sol}}{L\Delta Z} T = \frac{Q(t, x)}{L}, & (t, x) \in (0, t_F) \times \Sigma, \\ \lambda_{pow}.\nabla T \cdot n = 0, & (t, x) \in (0, t_F) \times \partial\Sigma \\ T(0, x) = T_{init}(x) & x \in \Sigma. \end{cases}$$

$$\text{with } Q(t, x) = P \exp \left( -\delta |x - u(t)|^2 \right)$$

$$\begin{cases} \dot{u}(t) = V\tau(t) & t \in [t_1, t_F] \\ u(t_1) = \tilde{u}. \end{cases}$$

# Optimal control of the line (Wendl, Pesch, and Rund (2010))

**Control of the line:** angle  $\theta$ , formed by the horizontal and the tangent at each point.



$$\min_{\theta, t_F, \tilde{u}} J = \Lambda_F(t_F) + \Lambda_\Phi(C_\Phi) + \Lambda_M(C_M),$$

while satisfying:

$$\begin{cases} \rho_{pow}.Cp,pow.\partial_t T - \nabla \cdot (\lambda_{pow}.\nabla T) + \frac{\lambda_{sol}}{L\Delta Z} T = \frac{Q(t,x)}{L}, & (t, x) \in (0, t_F) \times \Sigma, \\ \lambda_{pow}.\nabla T \cdot n = 0, & (t, x) \in (0, t_F) \times \partial\Sigma, \\ T(0, x) = T_{init}(x) & x \in \Sigma. \end{cases}$$

with  $Q(t, x) = P \exp(-\delta|x - u(t)|^2)$ , where the path equation  $u$  is given by:

$$\begin{cases} \dot{u}(t) = VF(\theta(t)) = V(\cos(\theta(t)), \sin(\theta(t))), & \forall t \in (t_1, t_F) \\ u(t_1) = \tilde{u} & \end{cases}$$

# Results:

**Values: (not realistic but efficient to test the algorithm)**

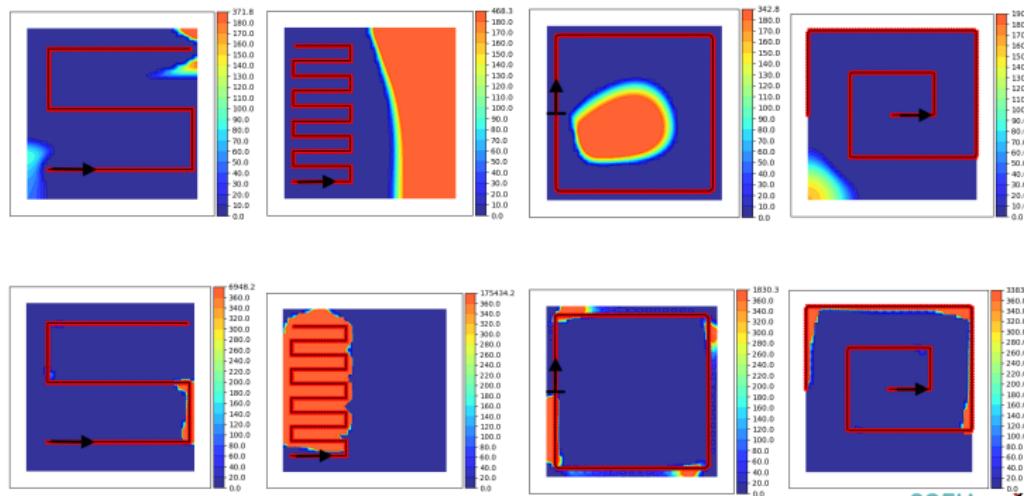
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$$\rho_{sol.} = \rho_{pow.} = 8000 \text{ kg.m}^{-3},$$

$$c_{sol.} = c_{pow.} = 450 \text{ J.kg}^{-1}.K^{-1}$$

$$L = 10 \text{ cm}, \quad \Delta Z = 10 \text{ cm}, \quad P = 76800000 * (10^4) \text{ W.m}^{-2},$$

$$T_\phi = 773 \text{ K}, \quad T_{init} = 303 \text{ K.}, \quad T_M = 2773, \quad p = 8.$$



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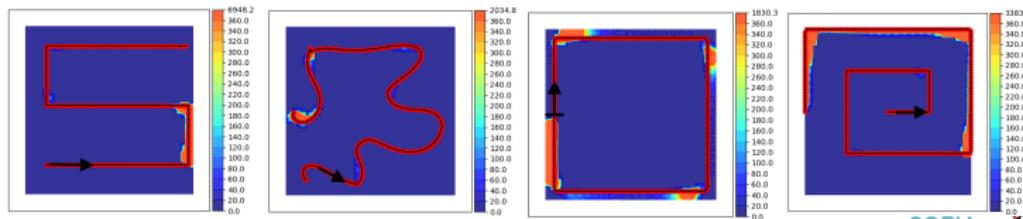
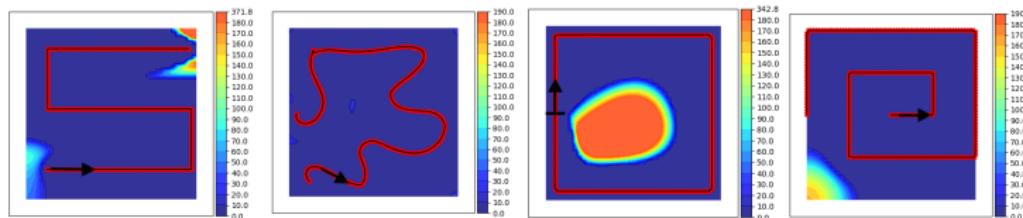
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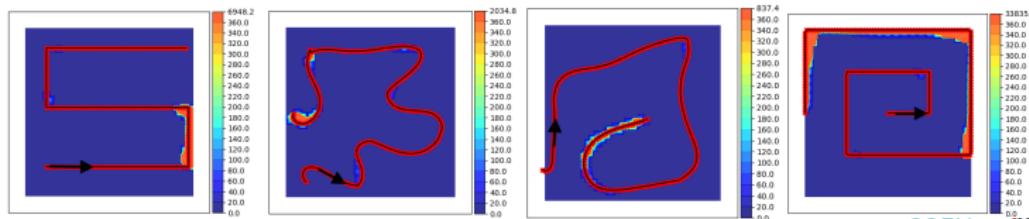
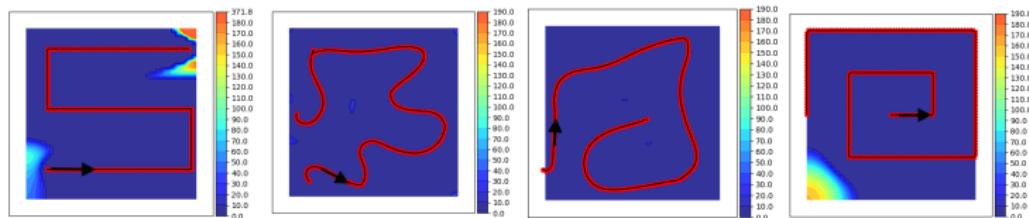
$$\lambda_{sol.} = 10000 \text{ W.m}^{-1}\text{K}^{-1}, \quad \lambda_{pow.} = 10000 \text{ W.m}^{-1}\text{K}^{-1},$$

$$\rho_{sol.} = \rho_{pow.} = 8000 \text{ kg.m}^{-3},$$

$$c_{sol.} = c_{pow.} = 450 \text{ J.kg}^{-1}\text{.K}^{-1}$$

$$L = 10\text{cm}, \quad \Delta Z = 10\text{cm}, \quad P = 76800000 * (10^4) \text{ W.m}^{-2},$$

$$T_\phi = 773\text{K}, \quad T_{init} = 303\text{K.}, \quad T_M = 2773, \quad p = 8.$$



# Results:

**Values: (not realistic but efficient to test the algorithm)**

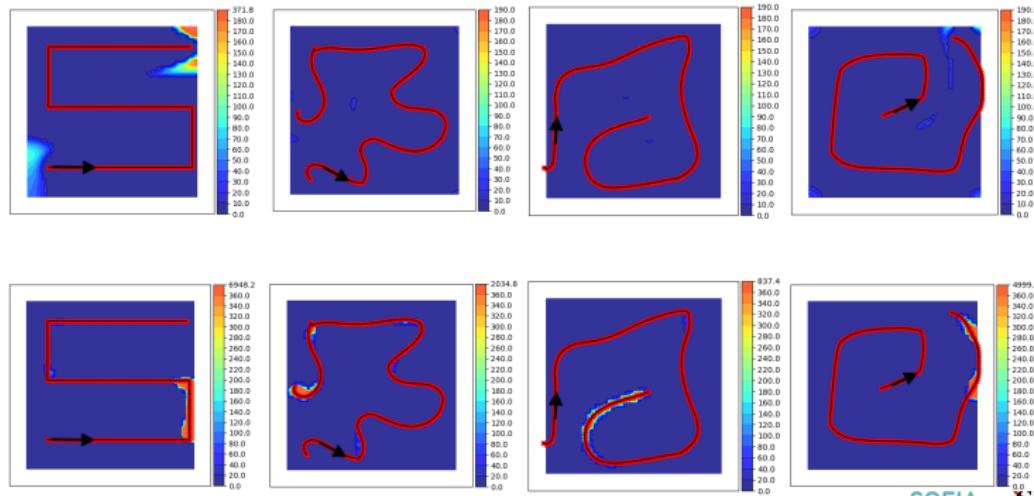
$$\lambda_{sol.} = 10000 \text{ W.m}^{-1}\text{K}^{-1}, \quad \lambda_{pow.} = 10000 \text{ W.m}^{-1}\text{K}^{-1},$$

$$\rho_{sol.} = \rho_{pow.} = 8000 \text{ kg.m}^{-3},$$

$$c_{sol.} = c_{pow.} = 450 \text{ J.kg}^{-1}.K^{-1}$$

$$L = 10 \text{ cm}, \quad \Delta Z = 10 \text{ cm}, \quad P = 76800000 * (10^4) \text{ W.m}^{-2},$$

$$T_\phi = 773 \text{ K}, \quad T_{init} = 303 \text{ K}, \quad T_M = 2773, \quad p = 8.$$



## Conclusion and perspectives

# Perspectives

## Short terms perspectives:

- steady case:
  - adding more realistic constraints (geometrical, thermal et mechanical),
  - allow for the splitting of the path and gathering many,
  - adapt the curve meshing to the industrial requirements,
  - make the 2D case evolve to a layer by layer 3D optimization.
- unsteady case:
  - improve the optimal control model,
  - consider the dependence in time of the physical coefficients,
  - perspectives from the steady case.

## Long term perspectives:

- coupling shape optimization to path optimization,
- optimize a line in 3D.

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