

PATH OPTIMIZATION FOR THE LASER POWDER BED FUSION ADDITIVE

MANUFACTURING PROCESS

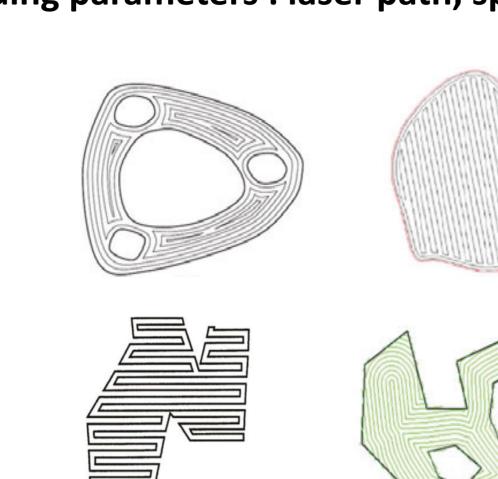
Mathilde BOISSIER^{1,2}, Grégoire ALLAIRE¹, Christophe TOURNIER² ¹ CMAP, Ecole Polytechnique, France ² LURPA, ENS Paris-Saclay, France



CONTEXT

Decomposition in layers

Choice of building parameters: laser path, speed, power



Building process laser roller and scraper printed object powder

Evaluation of the process

drawbacks in the item's quality (thermal expansion, residual stresses, ...)

evaluation of the process's speed (kinematics)

2D MODEL

G. Allaire and al., Shape optimization of a layer-by-layer

mechanical constraint for additive manufacturing, C. R. Math.

Acad. Sci. Paris 355 (2017) 699–717

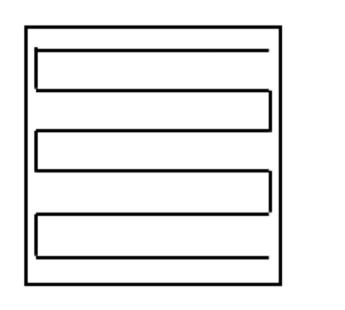
Constraints to satisfy:

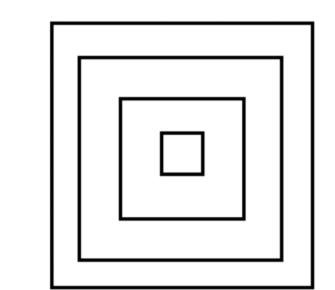
$$\begin{cases} \dot{u}(t) = v(t)\tau(t) & t \in (0, t_F) \\ u(0) = u_0 \end{cases}$$

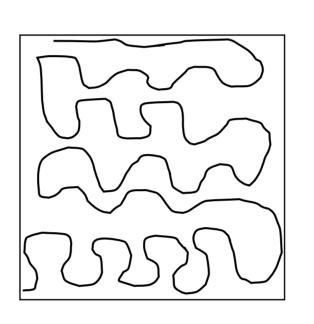
Heat Equation:

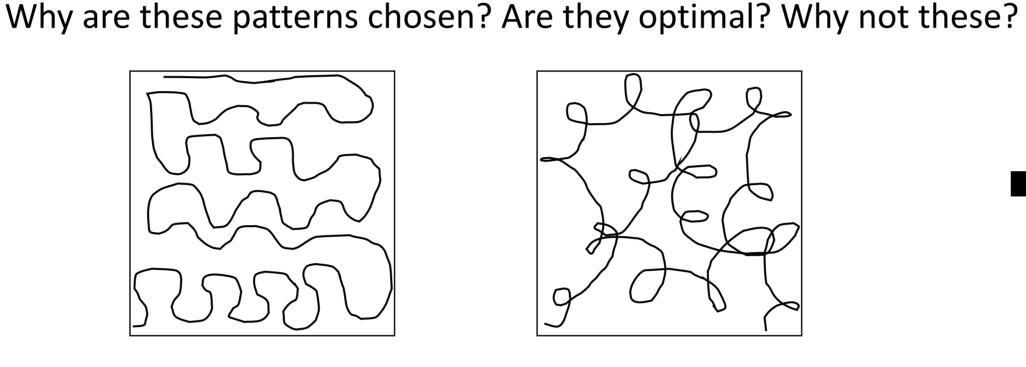
OBJECTIVE

Existing laser paths based on predefined patterns.









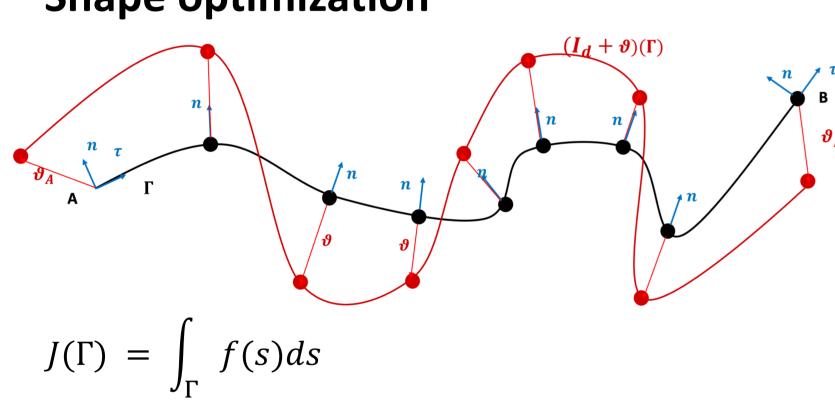
Optimize the laser path to improve both the mechanical and kinematic properties of the process, without basing it on any pattern.

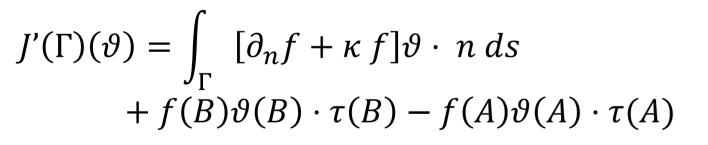
STEADY CASE (source applied on the whole path: heating thread)

$$\min_{\Gamma} J(\Gamma) = \int_{\Gamma} ds$$
 under the constraints

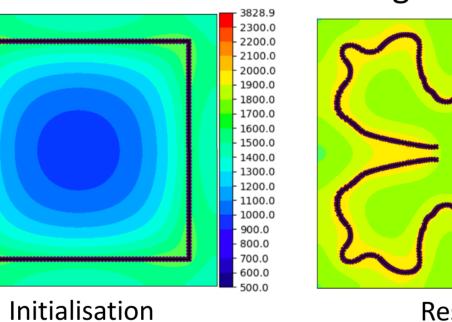
$$\begin{cases} -\nabla \cdot (\lambda_{pow} \nabla T) + \frac{\lambda_{sol}}{L\Delta Z} T = \frac{P}{L} \mathbf{1}_{\Gamma}, & x \in \Sigma, \\ \lambda_{pow} \nabla T \cdot n = 0 & x \in \partial \Sigma. \end{cases}$$

Shape optimization

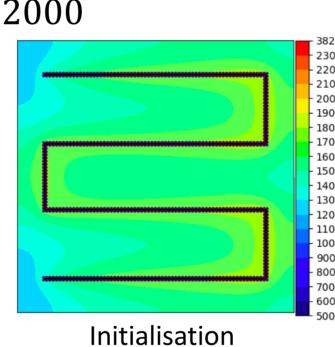




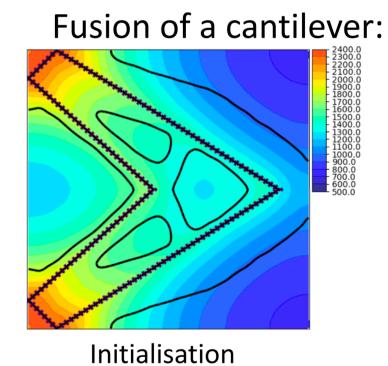
Fusion of the whole rectangle: 1700 < T < 2000

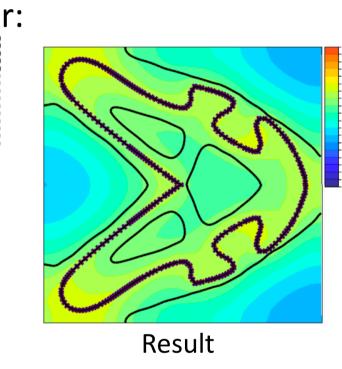


Result



Result





Future work

- Adding constraints
 - Allow for splitting a path and gathering paths
 - 3D optimization: consider the evolution of the path depending on the layer

UNSTEADY CASE (source moving along the path)

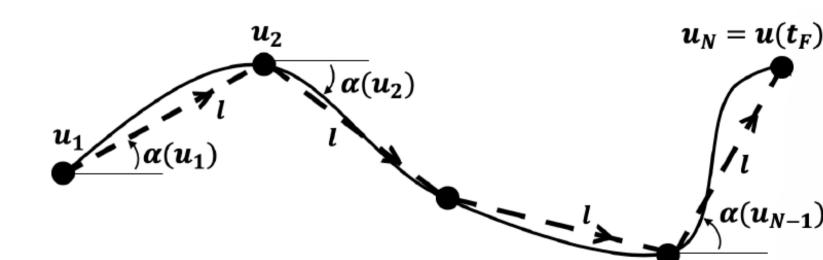
Assumptions

- fixed velocity V (constant along the path)
- fixed power P (constant along the path)

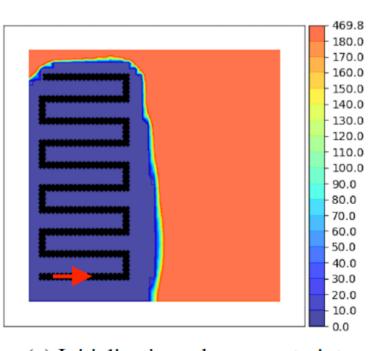
Optimal control problem $\min_{\Gamma} J(\alpha) = t_F + \int_{\Sigma} \left[(T_{\Phi} - ||T(.,x)||_{L^2([0,t_F])})^+ \right]^2 dx + \int_0^{t_F} \int_{\Sigma} [(T(t,x) - T_M)^+]^2 dx dt$

Results (Values from L. Van Belle, Analyse, Modélisation et Simulation de l'apparition de contraintes en Fusion Laser Métallique, yon, INSA, Nov. 2013)

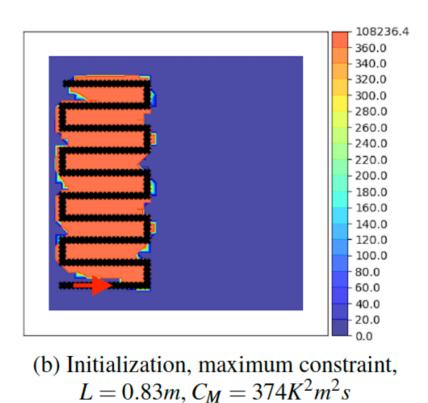
 $\dot{u}(t) = (\cos(\alpha(t), \sin(\alpha(t))) \quad t \in (0, t_F)$ with T solution of the heat equation, where $Q(t,x) = Pe^{-\delta(x-u(t))^2}$ and $u(0) = u_0$

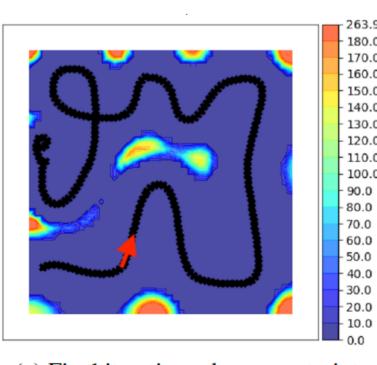


Results

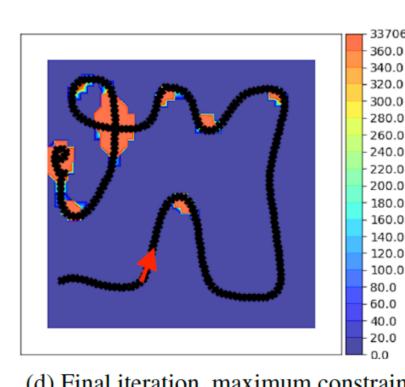


(a) Initialization, phase constraint, $L = 0.83m, C_{\phi} = 4245K^2m^2$





(c) Final iteration, phase constraint, $L = 0.86m, C_{\phi} = 52K^2m^2$



(d) Final iteration, maximum constraint, $L = 0.86m, C_M = 72K^2m^2s$

Future work

- Improve the results
- Same work than for the steady case

PERSPECTIVES

- coupling the shape and path optimization
- optimizing a line in a 3D domain

REFERENCES

- M. Megahed et al. "Metal Additive-Manufacturing Process and Residual Stress Modeling", Integrating Materials and Manufacturing Innovation 5.1 (Dec. 2016), p. 4.
- G. Allaire and L. Jakabčin. "Taking into Account Thermal Residual Stresses in Topology Optimization of Structures Built by Additive Manufacturing", Mathematical Models and Methods in Applied Sciences 28.12 (2018), pp. 2313–2366.
- J. L. Lions. Optimal Control of Systems Governed by Partial Differential Equations. Vol. 170. Springer (1971).
- S. Wendl, H. J. Pesch, and A. Rund. "On a State-Constrained PDE Optimal Control Problem Arising from ODE-PDE Optimal Control", Recent Advances in Optimization and Its Applications in Engineering. (2010), pp. 429-438.